

Al-Fe-Ni (Aluminum-Iron-Nickel)

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This technologically important system has been investigated experimentally, assessed thermodynamically, reviewed and updated a number of times. Table 1 gives the details of selected, more-recent studies. Very recently, [2009Zha] carried out a revised thermodynamic analysis, combining new calorimetric measurements of thermodynamic properties, first-principles calculations and the CALPHAD approach. This work will be reviewed briefly here.

Binary Systems

The Al-Fe phase diagram [1993Kat] shows that the face-centered cubic (fcc) solid solution based on Fe is restricted by a γ loop. The body-centered cubic (bcc) solid solution exists in the disordered $A2$ form, as well as the ordered $B2$ and $D0_3$ forms. Apart from the high temperature phase ϵ ($D8_2$, Cu_5Zn_8 -type cubic; stable between 1232 and 1102 °C), there are three other intermediate phases in this system: FeAl_2 (triclinic), Fe_2Al_5 (70-73 at.% Al, orthorhombic), and $\text{Fe}_4\text{Al}_{13}$ (74.5-76.6 at.% Al, monoclinic). The Al-Ni phase diagram [1993Oka] shows five intermediate phases: NiAl_3 ($D0_{11}$, Fe_3C -type orthorhombic), Ni_2Al_3 ($D5_{13}$ -type hexagonal), NiAl ($B2$, CsCl-type cubic, denoted β), Ni_5Al_3 (Ga_3Pt_5 -type orthorhombic), and Ni_3Al ($L1_2$, AuCu_3 -type cubic, denoted γ). The Fe-Ni phase diagram is characterized by a very narrow solidification range with a peritectic reaction at 1514 °C, that yields the Fe-based fcc

solid solution. A continuous fcc solid solution γ is stable over a wide range of temperature. At 517 °C, an ordered phase FeNi_3 forms congruently from γ .

Ternary Phases

Three ternary phases are known in this system. $(\text{Fe,Ni})_2\text{Al}_9$ (also written as FeNiAl_9) has the Co_2Al_9 -type of monoclinic structure, with lattice parameters of $a = 0.62406$, $b = 0.62993$, $c = 0.85992$ nm, and $\beta = 95.129^\circ$ at $\text{Fe}_{0.7}\text{Ni}_{1.3}\text{Al}_9$ [2007Chu1]. $\text{Fe}_3\text{NiAl}_{10}$ has the Co_2Al_5 -type of hexagonal structure, with $a = 0.770937$ nm and $c = 0.767947$ nm at $\text{Fe}_{2.67}\text{Ni}_{1.43}\text{Al}_{9.9}$ [2007Chu1]. $(\text{Fe,Ni})_2\text{Al}_9$ was denoted as τ_2 by [2007Chu1], [2008Rag], [2009Rag1], and [2009Rag2] and as τ_1 by [2005Cac], [2007Zha], and [2009Zha]. $\text{Fe}_3\text{NiAl}_{10}$ was denoted as τ_1 by [2007Chu1], [2008Rag], [2009Rag1], and [2009Rag2] and as τ_2 by [2005Cac], [2007Zha], and [2009Zha]. This mix-up of terminology is unfortunate. Since this update is primarily based on the work of [2009Zha], the nomenclature adopted by [2009Zha] for τ_1 and τ_2 will be used, i.e., $\text{FeNiAl}_9 = \tau_1$ and $\text{Fe}_3\text{NiAl}_{10} = \tau_2$. The third ternary phase is a decagonal, quasicrystalline phase with a periodicity of ~ 0.4 nm. It is stable between 930 and 847 °C and occurs at the approximate composition $\text{Fe}_5\text{Ni}_{24}\text{Al}_{71}$ [2007Chu1]. It will be denoted as D here (denoted q by [2007Chu1] and τ_3 by [2009Zha]).

Table 1 Details of selected previous studies of the Al-Fe-Ni system

Reference	Nature of study	Evaluated data presented
[1988Ray]	Review	Liquidus and solidus projections, isothermal sections at 1250, 950, 850, 750, and 600 °C, reaction sequence
[1994Rag]	Update	Isothermal sections at 1050 and 950 °C, vertical section along $\text{Ni}_3\text{Fe-Ni}_3\text{Al}$ join
[2005Cac]	Review	Partial liquidus projections, isothermal sections at 1350, 1250, 1150, 950, 850, 750, and 620 °C, four vertical sections, reaction sequence
[2005Rag]	Update	Isothermal sections at 1127 and 1100 °C
[2006Ele]	Review	Liquidus projection, isothermal sections at 1350, 1250, 1150, 1050, 950, 850, and 750 °C, vertical sections along $\text{Ni}_3\text{Al-Ni}_3\text{Fe}$ and FeAl-NiAl joins
[2006Rag]	Update	Isothermal sections at 1300, 1100, and 900 °C, vertical section along $\text{Ni}_3\text{Fe-Ni}_3\text{Al}$ join
[2007Chu1]	Experimental	Liquidus projection, isothermal sections at 850 °C, vertical sections at 80, 75, 71.5, 67, and 60 at.% Al
[2007Chu2]	Experimental	Vertical sections along the $\text{Ni}_3\text{Al-Ni}_3\text{Fe}$ join
[2007Zha]	Thermodynamic analysis, experimental	Computed liquidus projection, computed isothermal sections at 1250, 1050, 950, and 850 °C, three computed vertical sections at 1 mass% Ni, 1 mass% Fe, and along $\text{Ni}_3\text{Fe-Ni}_3\text{Al}$ join, respectively
[2008Chu]	Experimental	Isothermal sections in the Al-lean region at 1200, 1100, 1000, and 900 °C
[2008Rag]	Update	Liquidus projection, isothermal sections at 850 °C, Vertical sections at 71.5 and 60 at.% Al, reaction sequence
[2008Zha]	Experimental	Isothermal sections at 850 and 627 °C
[2009Rag1]	Update	Isothermal sections at 1200, 1100, 1000, 900, 850, and 627 °C, vertical section along $\text{Ni}_3\text{Fe-Ni}_3\text{Al}$ join
[2009Rag2]	Update	Isothermal sections at 1250, 1050, 950, and 850 °C, a vertical section along the $\text{Ni}_3\text{Fe-Ni}_3\text{Al}$ join

Computed Ternary Phase Equilibria

A thermodynamic assessment of this system was reported recently by [2007Zha] and reviewed by [2009Rag2]. [2009Zha] made a revised assessment of the system. New experimental results on the phase equilibria by [2007Chu1], [2007Chu2], [2008Chu], and [2008Zha] were included in the optimization, in addition to those used by [2007Zha]. Using high temperature reaction calorimetry, the

enthalpies of formation of FeNiAl_9 and $\text{Fe}_3\text{NiAl}_{10}$ were determined by [2009Zha]. With starting metal powders of 99.97% Al, 99.99% Fe, and 99.996% Ni, pellets of the above ternary compositions were prepared for the calorimetric experiments. First-principles calculations were performed to obtain the enthalpies of formation of the end-members of the ternary phases $(\text{Fe,Ni})_2\text{Al}_9$ and $(\text{Fe,Ni})_2\text{Al}_5$, varying the composition of the sublattice housing Fe and Ni. Calculations were done also to estimate

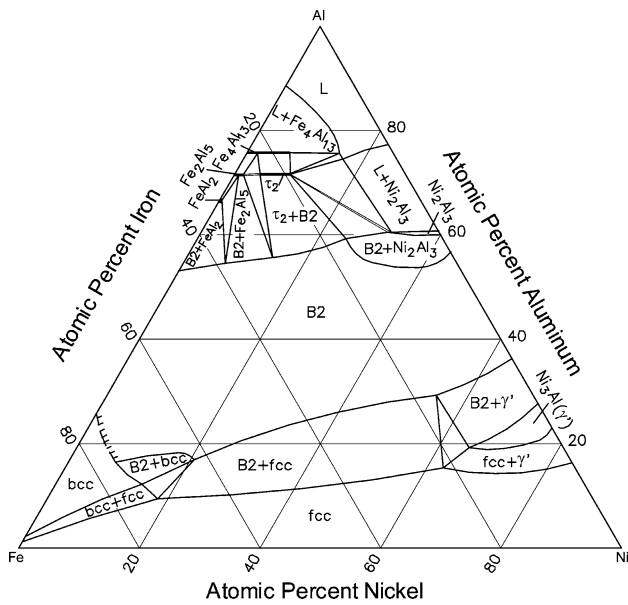


Fig. 1 Al-Fe-Ni computed isothermal section at 1050 °C [2009Zha]

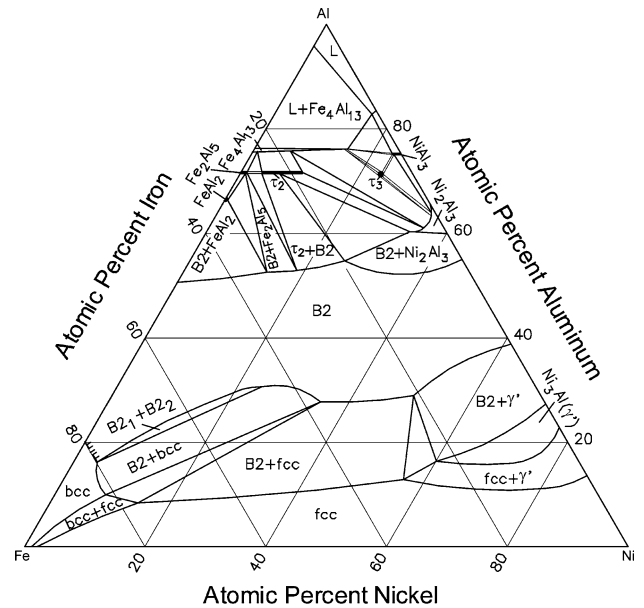


Fig. 3 Al-Fe-Ni computed isothermal section at 850 °C [2009Zha]

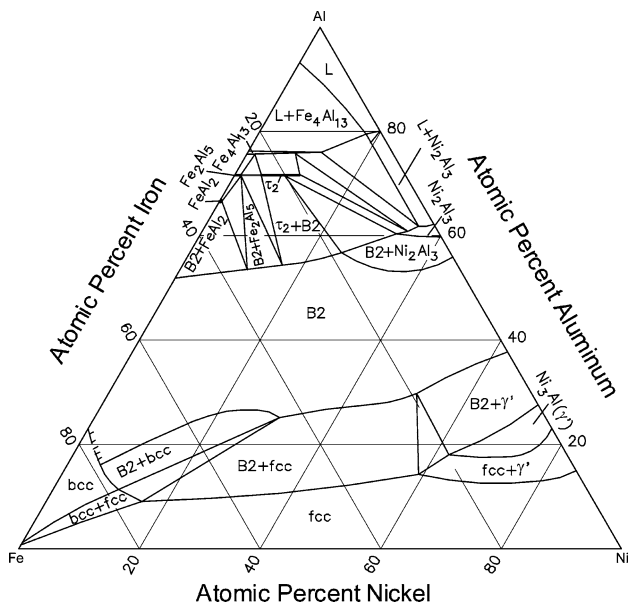


Fig. 2 Al-Fe-Ni computed isothermal section at 950 °C [2009Zha]

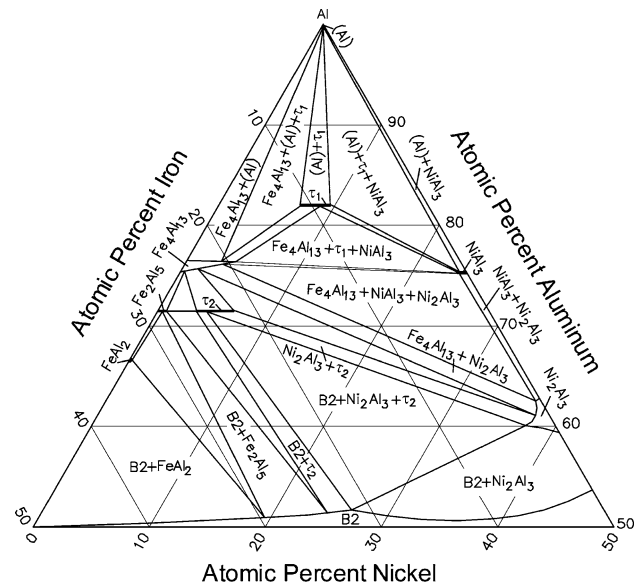


Fig. 4 Al-Fe-Ni computed isothermal section at 627 °C for Al-rich alloys [2009Zha]

the enthalpies of formation of Al_2FeNi , AlFe_2Ni , and AlFeNi_2 with the $L1_2$ ordered structure. The calculations were based on the generalized gradient approximation method. For details, see [2009Zha]. In all the cases, the values obtained experimentally, by first-principles calculation and by CALPHAD optimization showed reasonable agreement.

For the binary systems, [2009Zha] used the published descriptions from the literature. For the binary compounds $\text{Fe}_4\text{Al}_{13}$, Fe_2Al_5 , FeAl_2 and Ni_2Al_3 and NiAl_3 , which exhibit ternary solubility, appropriate sublattice models were used. The ternary solubility in ϵ and Ni_5Al_3 was ignored. Sublattice models of the type $(\text{Fe,Ni})_2\text{Al}_9$ and $(\text{Fe,Ni})_2\text{Al}_5$ were used for the ternary compounds τ_1 and τ_2 , respectively. The high-temperature, quasicrystalline phase D (τ_3 in [2009Zha]) was treated as a stoichiometric compound. The liquid, disordered fcc, and disordered bcc phases were treated as substitutional solutions. The magnetic contribution to the Gibbs energy was taken into account. An ordering term was added to the Gibbs energy term of the disordered bcc and fcc phases, in order to describe the $B2$ and $L1_2$ ordered phases, respectively. The calculated thermodynamic properties were used as inputs for the optimization. The optimized interaction parameters were listed.

The isothermal sections for the entire composition range at 1050, 950, and 850 °C computed by [2009Zha] are shown in Fig. 1-3. The agreement with the experimental results from various sources is satisfactory. To preserve

clarity, the experimental data points are not included in the figures. The decagonal phase D, which forms peritectically at 928 °C and decomposes eutectoidally at 848 °C, is present only in Fig. 3. A miscibility gap is seen in the $B2$ phase at 850 °C. Figure 4 is the computed isothermal section at 627 °C for Al-rich alloys, which was compared with the experimental section of [2008Zha]. Figures 5 and 6 show the partial isothermal sections at 1200 and 900 °C for Al-lean alloys. Here again, the agreement with the experimental data from various sources (not shown) was found to be satisfactory.

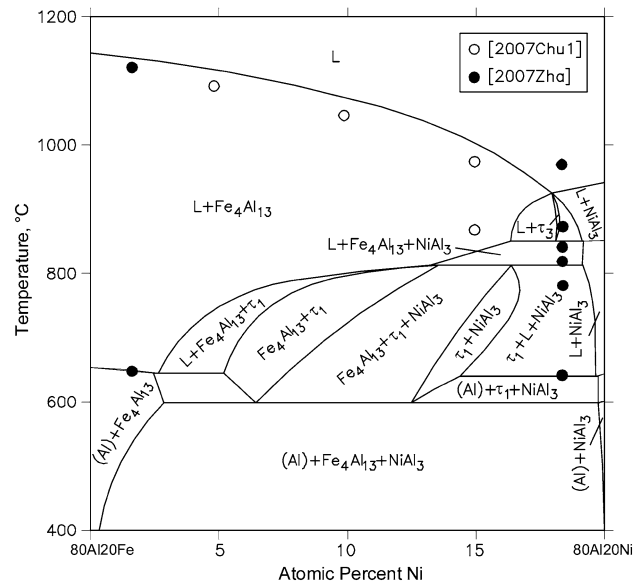


Fig. 7 Al-Fe-Ni computed vertical section at 80 at.% Al [2009Zha]

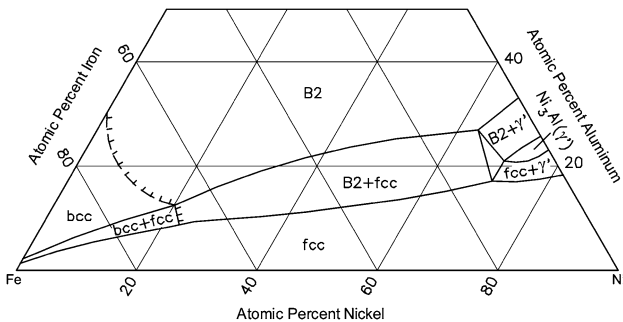


Fig. 5 Al-Fe-Ni computed isothermal section at 1200 °C for Al-lean alloys [2009Zha]

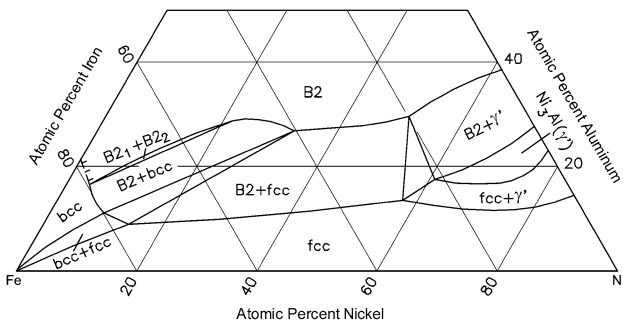


Fig. 6 Al-Fe-Ni computed isothermal section at 900 °C for Al-lean alloys [2009Zha]

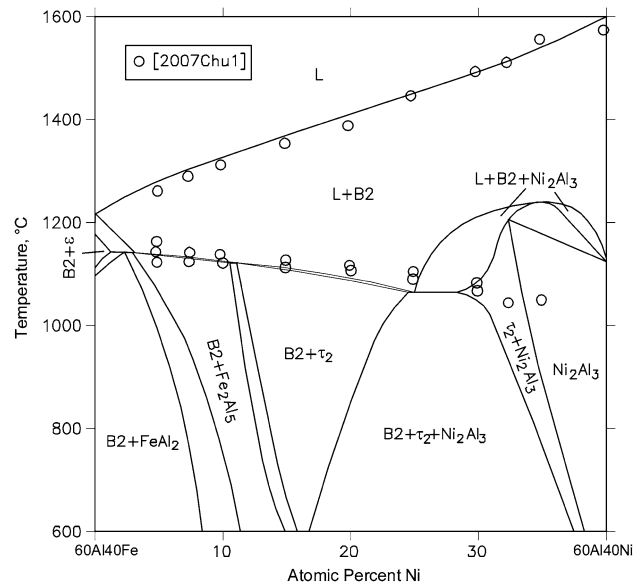


Fig. 8 Al-Fe-Ni computed vertical section at 60 at.% Al [2009Zha]

Section II: Phase Diagram Evaluations

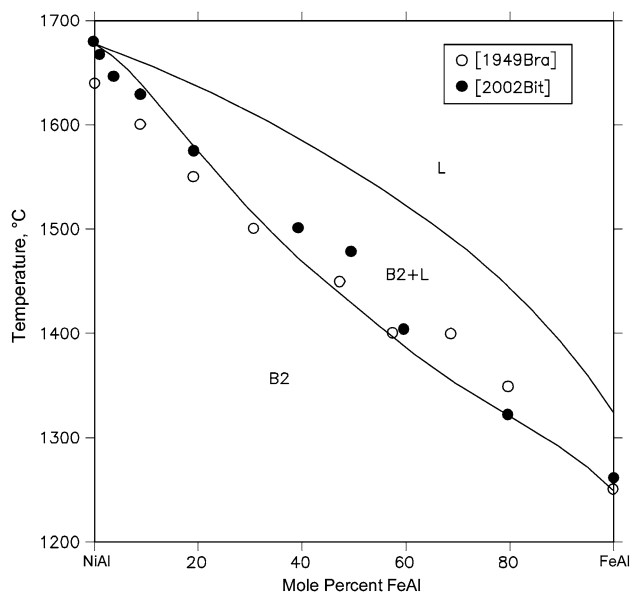


Fig. 9 Al-Fe-Ni computed vertical section along the NiAl-FeAl join [2009Zha]

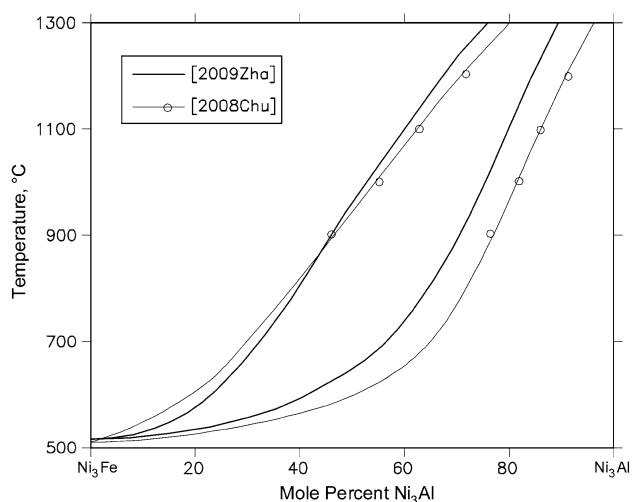


Fig. 10 Al-Fe-Ni computed vertical section along the Ni₃Fe-Ni₃Al join [2009Zha]

Four computed vertical sections at 80, 60, and 50 at.% Al and at 75 at.% Ni, respectively, are shown in Fig. 7-10. The sections in Fig. 7 and 8 are compared with the results of [2007Chu1] and [2007Zha] and the agreement is satisfactory. The same is seen in Fig. 9, where the computed section is compared with the data of [1949Bra] and [2002Bit]. In Fig. 10, the vertical section along the Ni₃Fe-Ni₃Al join computed by [2009Zha] is compared with the most recent experimental results of [2008Chu] from EPMA measurements. The experimental data points from various other sources indicated by [2009Zha] show a wide scatter and are not shown in Fig. 10. [2009Zha] also computed a liquidus projection and a reaction sequence for solidification

reactions. The computed invariant reactions and their temperatures generally agree with those reported by [2007Chu1] and reviewed in the update by [2008Rag], but with some differences.

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